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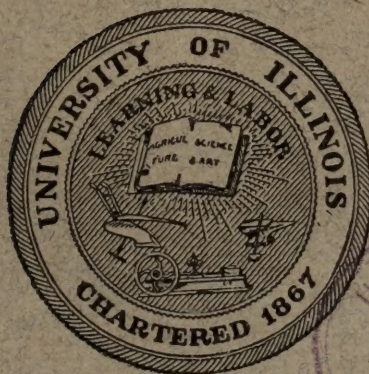
PASSENGER TRAIN RESISTANCE

BY

EDWARD C. SCHMIDT

AND

HAROLD H. DUNN



BULLETIN No. 110

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UNIVERSITY OF ILLINOIS
ENGINEERING EXPERIMENT STATION

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BY

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ENGINEERING EXPERIMENT STATION

PUBLISHED BY THE UNIVERSITY OF ILLINOIS, URBANA



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PASSENGER TRAIN RESISTANCE

I. INTRODUCTION

1. *Preliminary Statement.*—The Department of Railway Engineering of the University of Illinois has for some years carried on experiments to determine the tractive resistance of steam railway trains and electric railway motor cars.* The results relating to steam railways thus far published have applied only to freight trains. This bulletin presents for the first time the results of the experiments with passenger trains. These experiments were begun in 1908 on light local trains and were resumed during the spring and summer of 1916 on heavy equipment in through passenger service.

The results here presented define the resistance of the trains tested throughout the ordinary range of speed of passenger trains. The fact is also made clear that in passenger as in freight trains the resistance expressed in pounds per ton varies with the average weight of the cars composing the train, being less for trains made up of heavy cars than it is for trains of light cars. As regards freight train resistance, this influence of car weight has been recognized for some years, and this recognition found application in freight service in the making of tonnage ratings even before complete experimental data were at hand. Today tonnage ratings almost universally embody distinctions based upon this influence of car weight.

It has always seemed likely that the specific resistance of passenger trains was similarly affected by the weight of the cars in the train. Notwithstanding this probability, however, the influence of car weight has frequently been ignored in dealing with problems in passenger train resistance. It is embodied in only a few of the formulas currently used for that purpose, and even in some of these its influence is recognized only to the extent to which it affects the air

*See Bulletin 43, entitled "Freight Train Resistance: Its Relation to Car Weight," 1910, Bulletin 59, entitled "The Effects of Cold Weather upon Train Resistance and Tonnage Rating," 1912, Bulletin 74, entitled "The Tractive Resistance of a 28-ton Electric Car," 1914, and Bulletin 92, entitled "The Tractive Resistance on Curves of a 28-ton Electric Car," 1916, of the Engineering Experiment Station of the University of Illinois.

resistance component of net resistance, its effect on journal and rolling resistance being neglected. This situation has arisen primarily because of the lack of experimental data applying to passenger cars of different weights, and because the problems requiring the prediction of passenger train resistance have not the economic importance of similar problems arising in connection with freight trains. The error involved by ignoring car weight is not, however, so great in the former case as in the latter; for while passenger cars ordinarily vary in gross weight only from about thirty-five to sixty-five tons, the corresponding range in freight service is from about eighteen to ninety-eight tons. Despite this difference in the necessity of accurately determining resistance in the two instances, the prediction of passenger train resistance is nevertheless important, and data such as are here presented have been needed.

The results here set forth define the resistance of passenger trains made up of cars ranging in average weight from thirty-three to seventy-one tons, and, it is believed, present for the first time full experimental data showing the influence of car weight on the resistance of entire steam railroad passenger trains throughout the range of car weight now prevalent in American practice.* Throughout this bulletin the terms "resistance," "net resistance," and "specific resistance" mean the number of pounds of tractive force required for each ton of train weight in order to keep the train moving at uniform speed on straight level track. Ordinarily these terms apply to resistance in still air. Here, however, they include the effects on resistance of such winds as prevailed during the tests, which, as later appears, were from various directions and of velocities as high as thirty-one miles per hour. The bulletin deals exclusively with the resistance of the cars alone—locomotive and tender resistance were not measured and are not discussed.

The results of the last eighteen tests included in this report were separately summarized and discussed in a paper on "Passenger Train Resistance" published in February, 1917 in Bulletin 194 of the American Railway Engineering Association.

2. *Acknowledgments.*—Through the courtesy of W. L. PARK, Vice President, and R. W. BELL, General Superintendent of Motive

*Data concerning the resistance of two trains composed of cars of two different weights (46.2 tons and 62.7 tons) are given in Bulletin No. 26 of the Pennsylvania Railroad Company Test Department.

Power of the Illinois Central Railroad, the tests were made on the lines of that company between Champaign and Centralia, Illinois, and by means of a dynamometer car which since 1900 has been jointly owned by the Railroad Company and the University. The interest and the coöperation of E. H. BAKER, Trainmaster at Champaign, under whose immediate direction the test car was handled, are also gratefully acknowledged.

II. SUMMARY

At the expense of some duplication of statement, the following summary is presented at this point in order to provide a general view of the work.

3. *The Trains.*—The tests were undertaken to measure the resistance of passenger trains at all speeds up to seventy miles per hour and for average car weights varying throughout the entire current range in weight. The chief characteristics of the twenty-eight trains tested were as follows:

	Minimum	Maximum
Total weight (excluding locomotive and tender),		
tons	138	727
Number of cars in the train	4	12
Average gross weight per car, tons	33.6	71.1

Nine of these trains were in "local" service, the others in "through" service. Of the 240 cars composing these twenty-eight trains, 178 had six-wheel trucks, and 62 had four-wheel trucks.

4. *The Track.*—The experiments were made upon well constructed and well maintained main line track, nearly all of which is laid with either 85-pound or 90-pound rail. Except through station grounds where screenings or cinders are used for ballast, the track is ballasted with broken stone.

5. *The Results.*—The average values of the resistance of the trains tested are defined by the curves of Fig. 9. From these curves has been prepared Table 3, which shows probable average values of resistance for passenger trains composed of cars varying in weight from thirty to seventy-five tons, and at speeds ranging from five to seventy-five miles per hour. Individual trains will occasionally be met with whose general average resistance will exceed the values previously defined by from 8 to 10 per cent.

The tests were made in fair and moderate or warm weather during which the maximum wind velocity encountered at any time was, with one exception, twenty-five miles per hour. The results are probably safely applicable to passenger trains running under like conditions of track and weather. They should not, however, be applied without modification to trains running under widely different conditions.

III. THE TRAINS, THE TRACK AND THE TEST CAR

6. *The Trains Tested.*—The twenty-eight passenger trains included in the report were tested in two series. Series I comprises ten tests which were made in 1908-1909 in conjunction with freight resistance tests then in progress. At that time the test car was operated from Champaign to Mattoon, Illinois, in freight service and it was usually returned in local passenger train No. 24 from Mattoon to Champaign. The test car was operated upon one occasion at this period in through train No. 5, and Series I includes, therefore, nine runs with train 24 and one with train 5. The average weight of the cars in train 24 varied during the nine tests then made only from 33.6 to 40.7 tons, and the results based on this limited range in weight did not warrant generalizations. The opportunity to continue the tests with heavy trains did not present itself until May of 1916 when the work was resumed and continued during the summer with trains No. 5 and No. 2. Eleven tests were then made with train No. 5, "Fast Mail," running from Champaign to Centralia, and seven tests with train No. 2, "Through Mail," running from Centralia to Champaign. These eighteen tests constitute Series 2.

Considering both series together the range in train weight was from 138 to 727 tons, in average car weight from 33.6 to 71.1 tons, and the number of cars per train varied from 4 to 12. For each of the three classes of trains the variations in train weight, car weight, number of cars, and truck construction were as follows:

Train No.	Number of Trains Tested	Gross Weight of Train, Tons		Average Weight per Car, Tons		Number of Cars in the Train		Number of Cars per Train Having 4-wheel Trucks	
		Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.
24	9	138.0	234.2	33.60	40.70	4	6	3	4
5	12	370.6	615.5	46.32	55.90	10	12	2	3
2	7	549.0	727.0	63.49	71.10	8	11	0	2

Similar data and other details concerning the make-up of each of the trains are presented in Table 1.

Train No. 24 is scheduled to cover the 45 miles from Mattoon to Champaign in 1 hour and 22 minutes, a schedule speed of 32.9 miles per hour. A typical running time for this train is 1 hour and 10 minutes, equivalent to a running speed of 38.6 miles per hour. Train No. 5 is allowed by the schedule 3 hours and 35 minutes to cover the 124.5 miles from Champaign to Centralia; thus its schedule speed is 34.8 miles per hour. Its running time is about 2 hours and 51 minutes, which corresponds to a running speed of 43.7 miles per hour. Train No. 2 is scheduled between Centralia and Champaign at 3 hours and 5 minutes, a schedule speed of 40.4 miles per hour. For this train a typical running time, 2 hours and 37 minutes, is equivalent to a running speed of 47.5 miles per hour.

In eight of the nine tests of train 24 the resistance of the dynamometer car itself is included in the records and its weight is included in the train weight. The weight of the test car, 29 tons, is however not greatly different from the average weight of the cars in this train and its inclusion has lowered only slightly the average car weight. The test car weight is likewise included in five of the tests with trains 2 and 5, and in these instances its relatively light weight has lowered appreciably the normal average car weight. In the remaining fourteen tests the dynamometer car was coupled with its measuring drawbar toward the rear of the train, and in these cases its own resistance is excluded from the test car records. Its weight is consequently excluded from the train weights and has not affected the normal average car weights.

The net weights of all cars were obtained from the records of the Illinois Central Railroad and the Pullman Company. To determine the car loads passengers were counted and allowed for at 140 pounds each; the weights of baggage and mail were estimated by personal inspection and count of the contents of each car; the weight of express was determined by reference to the bills, supplemented by inspection and estimate. The error entailed by these methods certainly does not exceed fifteen per cent of the weight of the load, and since among all the trains the maximum load amounted to only 6.6 per cent of the gross train weight, the maximum error in gross train weight itself caused by inaccuracies in the processes described is less than one per cent.

Of the three classes of trains tested, local train No. 24 had the lowest average car weight and, naturally, the highest proportion of

four-wheel truck cars. Of the 45 cars composing these nine local trains, 28 (or 62 per cent) had four-wheel trucks. In the twelve trains No. 5 there were included altogether 129 cars, of which 27 (or 21 per cent) were equipped with four-wheel trucks. Train No. 2 had the heaviest cars and the smallest proportion of four-wheel truck cars. The seven trains of this class included 66 cars, of which only 7 (or 10.6 per cent) had four-wheel trucks. All other cars in the three classes of trains had six-wheel trucks.

Since car weight affects the specific resistance, not only through its influence on air resistance, but through its influence on journal and rolling resistance as well, there is apparently an inconsistency in method in grouping—as is done in this report—trains including both four-wheel and six-wheel truck cars, and especially in thus grouping trains which have in their make-up different proportions of the two kinds of trucks. This apparent inconsistency, considering the purpose of the investigation, is not so objectionable as may appear. It was not possible under the conditions under which the tests were made to control the make-up of the trains. The tests had to be made in regular service and the trains had to be accepted with their usual make-up. This limitation has not defeated the main purpose of the tests, for they were undertaken, not to distinguish the resistance of four-wheel and six-wheel truck cars, but to measure the resistance of ordinary passenger trains of widely different average car weight; and wide variation in car weight carries with it, in American practice, a variation in truck construction similar to that encountered in the trains here discussed. Any train of 35 to 40 tons average car weight is sure to include in its make-up four-wheel truck cars,—and in about the proportion which prevailed in these tests. Even the heaviest through trains are likely occasionally to include a car or two with four-wheel trucks, as was the case with Train No. 2.

7. *The Track.*—The track, formerly part of one of the oldest single-track lines in the State, was converted about twenty years ago into a double-track road. The roadbed is in good condition and the drainage in general is excellent. The track was especially surveyed for the purposes of these tests.

Except on a few short stretches through station grounds, where cinders and screenings are used for ballast, both tracks are ballasted with broken limestone. The cross-ties, 6 inches by 8 inches by 8 feet,

are spaced about 20 inches between centers and are of treated red oak, treated soft wood or untreated white oak. Seventy miles of the southbound track are laid with 90-pound rail of American Railway Association section, while the remaining 54.5 miles are laid with 85-pound rail of American Society of Civil Engineers section; 98.6 miles of the northbound track are laid with 85-pound rail of American Society of Civil Engineers section, while the remaining 25.9 miles are laid with 90-pound rail of American Railway Association section. All rails are laid with broken joints supported on two ties. During eight months of the year there is employed in maintaining this portion of the road a force of men averaging one man per mile of track. During the remaining four months this force is reduced to one man for each two miles.

8. *The Test Car.*—The dynamometer car used in these experiments has been described in detail in Bulletin 43 of the Engineering Experiment Station of the University of Illinois and in the *Railway Age Gazette* for February 19, 1909. The recording apparatus within the car produces continuous graphical records of the gross resistance of the train, speed, time, brake cylinder pressure, wind direction, wind velocity, and location of mile posts and other reference points. A reproduction of one of the test car records is given in Bulletin 43 previously mentioned. When supplemented by an accurate profile and train data, these records permit the calculation of train resistance at any point or section on the road. The methods by which these calculations were made and the precautions observed to ensure accuracy are explained later.

IV. TEST CONDITIONS, METHODS AND CALCULATIONS

9. *Test Conditions.*—In Table 1 are set forth for each test the weather conditions, the average velocity and the direction of the wind, and the air temperatures prevailing at the beginning and at the end of the test. With only two exceptions the tests were made on fair days and in moderate or warm weather. The average air temperature varied from 40 degrees F. during one test to 93 degrees F. in another. The average wind velocity was 20 m. p. h. or less during all but three tests. During two tests the average wind velocity was 25 m. p. h. and on only one it was 31 m. p. h.

While the wind velocity was recorded for each test, the uncertainties regarding its influence have made a definite evaluation of its share of the total resistance impracticable. It has seemed necessary, therefore, to regard the wind velocity as one of the incidental variables which is likely to be met with in train operation and which should be included in the final resistance values. It has, accordingly, been included and the terms “resistance” and “specific resistance” as here used include the resistance due to such winds as prevailed during the tests.

10. *Test Methods.*—As has already been stated the tests were run in regular service, no attempt being made to modify schedules or to control speed. During each test the data cited in the description of the test car were produced and from them resistance was calculated for as great a variety of speeds as the records presented. These resistance values were then plotted in a diagram such as any one of the curves in Fig. 1, which shows for the train in question the relation between resistance and speed. The production of such a diagram was the immediate purpose of each test, and it was the expectation that when the resistance-speed curves of the individual tests were brought together, analysis of the curves would reveal the relations existing between train resistance and car weight.

The pressure in the brake cylinder was recorded merely to make it possible to distinguish the periods when the brakes were applied, it being obviously necessary to avoid such portions of the record when

TABLE 1

TRAIN DATA AND WEATHER CONDITIONS

Test Number	Date of Test	Weather	Air Temperature Degrees F.		Approximate Average Wind Velocity Miles per Hour	Range of Direction of the Wind with Respect to the Track ¹		Train Length Feet	Weights		Total Number of Cars in the Train	No. of Cars Having 2 Axles per Truck	No. of Cars Having 3 Axles per Truck	Kind of Cars						
			At Beginning of Test	At End of Test		From	To		Gross Train Weight Tons	Average Gross Weight per Car Tons				Test	Baggage and Express	Mail	Coach	Pullman	Diner	Special
1	10-31-08	Fair	60	60	11	+20° R	-81° R	300	202.9	40.58	5	3	2	1	1	1	2	2
2	11-7-08	"	50	55	13	+45° L	-88° L	300	203.5	40.70	5	3	3	1	1	1	1	2	2	...
3	11-21-08	"	62	60	8	+8° R	+39° R	300	185.1	37.02	5	3	3	1	1	1	2	2
4	1-23-09	"	66	70	20	+16° R	+39° R	345	234.2	39.03	6	3	3	1	1	1	1	2	2	...
5	1-28-09	Rainy	40	41	18	+28° R	+55° R	300	189.4	37.90	5	3	2	1	1	1	1	2	2	...
6	2-2-09	Fair	45	45	11	+0°	+33° L	300	185.5	37.10	5	3	3	1	1	1	1	2	2	...
7	3-12-09	Cloudy	41	41	11	+27° R	+60° R	300	185.6	37.12	5	3	3	1	1	1	1	2	2	...
8	3-27-09	Fair	40	45	13	+34° L	+68° L	330	168.0	33.60	5	4	4	1	1	1	1	2	2	...
9	4-17-09	"	74	71	31	+36° R	+59° R	255	138.0	34.50	4	3	3	1	1	1	1	2	2	...
10	7-8-08	"	50	60	14	+10° L	+22° L	480	370.6	46.32	8	2	6	...	2	3	2	1
11	5-25-16	"	82	86	700	604.5	54.96	11	2	9	...	6	2	2	1
12	5-25-16	"	86	90	20	-30° R	+55° R	700	570.0	51.80	11	2	9	...	6	2	2	1
13	6-9-16	"	72	72	15	-40° R	+25° R	700	615.5	55.90	11	2	9	...	4	4	2	1
14	6-9-16	"	72	69	10	-15° R	+10° R	640	551.3	55.13	10	2	8	...	3	4	2	1
15	6-9-16	"	72	69	10	-15° R	+10° R	640	727.0	66.10	11	1	10	...	1	1	3	4	1	...
16	6-22-16	"	75	77	660	538.5	49.04	11	2	9	...	5	2	2	1	...	1
17	6-22-16	"	77	80	20	-70° L	+25° R	660	562.0	51.18	11	3	8	...	6	2	2	1
18	6-22-16	"	83	82	20	-70° L	+25° R	520	588.2	65.29	9	1	8	...	1	1	2	3	1	...
19	6-22-16	"	82	81	20	-70° R	+15° R	580	634.9	63.49	10	2	8	...	1	1	3	3	1	...
20	7-6-16	"	88	90	25	+0°	+20° L	650	601.6	50.13	12	3	9	...	6	2	2	1
21	7-6-16	"	90	92	25	+0°	+10° L	580	535.2	48.65	11	3	8	1	5	2	2	1
22	7-6-16	"	92	91	20	+15° L	+65° R	690	618.0	68.66	9	1	7	...	1	1	3	3	1	...
23	7-6-16	"	91	90	20	+0°	+35° R	630	549.0	68.63	8	1	7	...	1	1	2	2	1	...
24	7-13-16	"	86	89	20	+15° L	+40° R	615	570.1	51.83	11	2	9	...	6	2	2	1	...	1
25	7-13-16	"	89	93	15	+5° R	+40° R	630	540.0	49.10	11	2	9	...	5	2	2	1	...	1
26	7-13-16	"	93	92	15	+30° L	+35° R	765	708.3	70.83	10	1	9	...	1	1	3	4	1	...
27	7-13-16	"	92	90	15	+60° R	+23° L	720	639.9	71.10	9	2	9	...	1	1	2	4	1	...
28	8-2-16	"	72	72	20	+25° L	+45° L	675	606.2	55.10	11	2	9	...	6	2	2	1

¹Direction is designated by the angle made with the track. A wind which has any component of its velocity helping the train forward is marked +; winds with opposing velocity components are marked -. Winds from the right side of the track are designated as R; from the left side as L; thus +40°R means a wind blowing from the rear and from the right hand side, whose direction makes an angle of 40 degrees with the track.

choosing sections for calculation. The wind velocity and direction relative to the test car were obtained by means of an anemometer and windvane mounted on its roof. When compounded with the known speed and direction of motion of the car, these data permit the determination of the actual wind direction and wind velocity with respect to the track. The location of the test car upon the road was defined by marking upon the chart the position of mile posts and stations at the moment they were passed by the car. This record makes it possible to correlate any portion of the chart with the road profile. In addition to the weight of the train there were recorded its length, the car names and numbers, and facts concerning the truck construction.

11. *Methods Employed in Calculating the Results.*—To produce for each train the resistance-speed curve referred to in the preceding section involves calculating the train resistance at various positions of the train upon the track, and the first step towards this end is the inspection of the test car record in order to select suitable points or sections at which the resistance may be calculated. The considerations of most importance in this selection are that the points represent finally as great a speed range as possible and that the speeds be approximately evenly distributed within this range. Points and sections were selected only where the entire train was running and continued to run upon straight track; resistance due to track curvature is therefore entirely eliminated. The data essential to the process of calculation are the drawbar pull of the engine, the train speed and its acceleration, the tonnage, and the profile. The pull and the speed, as previously stated, are determined from continuous curves drawn on the test car chart. Two processes have been used, designated here as method 1 and method 2. By method 1, the momentary values of pull, speed, acceleration, and grade were determined for a particular position of the train upon the road; by method 2 the average values of these quantities were determined for the period during which the test car was passing over a definite section of the track.

Under method 1, the point on the road having been chosen, the pull and the speed were found by direct readings from the chart. This pull divided by the tonnage gives the gross train resistance at this speed, and this gross resistance was then corrected for both acceleration and grade resistances. The acceleration was determined by graphical methods from the speed curve, and the grade was found by cor-

relating the position of the train with the profile. The points were all selected so that at the moment under consideration the entire train was on a nearly uniform grade. Method 1 results in momentary values of train resistance at the points considered.

By method 2 the average value of train resistance was determined for the period during which the test car at the head of the train was passing a selected section of the track. This track section corresponds to a certain length on the test car record. The section was selected so that the speed of the car when entering was nearly equal to its speed at exit and moreover so that no considerable variations in speed occurred during transit over the section. These portions of the chart having been chosen, the average pull was next found by determining the average ordinate of the curve of drawbar pull, and the average speed was found by means of the section length and the time record. Gross resistance in pounds per ton was next derived by dividing this value of pull by the tonnage, and this gross resistance was accordingly corrected for the resistances due to acceleration and grade, as in method 1. In this case the average acceleration is found by consideration of the speeds at entrance to and exit from the section. In order to correct for grade, the elevation of the center of gravity of the train was determined for that position of the train at which the test car entered the section, and again for the position at which the car left the section. The difference between these elevations establishes the effective average grade, which either helps or opposes the locomotive while the train passes the section. These elevations of the center of gravity of the train may not be determined with sufficient accuracy unless the train at the moment is on a practically uniform grade. The section limits were therefore so chosen. Method 2 results in a value of *average* train resistance for the *average* speed at which the train passes the section under consideration. It would be rigidly correct if train resistance varied uniformly with speed, in other words, if the curve showing the relation of resistance to speed were a straight line. This, of course, is not the relation, and the process accordingly gives results which are slightly in error. As previously stated, however, the section was chosen so that the difference between the speeds at entrance to and exit from the section was small, and for the speed range represented by this difference, the curve of train resistance deviates but little from a straight line. Such error as does result from the process is, therefore, very small, and is of no moment whatever when compared with

variations, due to natural causes, which occur in the resistance itself.

The two methods are fundamentally alike. Although the first is the less laborious, it requires the determination of acceleration at a point on the speed curve, which is occasionally difficult to make accurately. Method 2 is, accordingly, generally preferable, and it is also to be preferred because it deals with average values and therefore tends to eliminate from the results the incidental momentary variations which frequently occur in train resistance. Method 2 has consequently been used during these tests whenever it was possible to do so, but it has been necessary occasionally to resort to the use of method 1, especially for the determination of resistance at low speed, because in passenger service low speeds are rarely maintained for a long enough period to permit the use of the second method. Of all the resistance values included in this report only about 16 per cent were derived by method 1. These values are represented in the resistance speed diagrams by the circles, whereas values derived by method 2 are represented by the black dots.

In general the methods used during these tests were like those set forth in Bulletin 43 of the Engineering Experiment Station of the University of Illinois and described in detail in sections 11 to 15 and in Appendix 4 of that bulletin. The precautions taken to ensure accuracy which are there described, particularly in the determination of the acceleration corrections, were strictly observed in these experiments.

12. *The Derivation of the Resistance Curves.*—The calculations result, for each test, in a series of values of net train resistance at a variety of speeds. These values of resistance were plotted with respect to speed, and gave such a diagram as in Fig. 1. The curve, such as is shown there, was next drawn to express, for the test in question, the relation existing between resistance and speed. In order to draw this curve, the plotted points were assumed to be arranged in a number of groups, and for each group the averages of the values of speed and of resistance were determined. By these averages a new point or “center of gravity” of the group was then plotted. The curve was drawn by confining attention to the few points thus determined. The groups of points were arbitrarily selected so that the resulting “centers of gravity” would be distributed nearly equidistantly throughout the speed range. All curves presented in the report, except those shown in Fig. 9, were drawn by this process.

V. THE RESULTS OF THE TESTS

13. *Results of the Individual Tests.*—The immediate result of each test is a curve which shows for the train under consideration the relation existing between train resistance and speed. Fig. 1 includes such a curve for the train of test 1, in which the average weight of the cars was 40.58 tons. Similar curves for each of the twenty-eight trains tested are presented in Figs. 1 to 5 inclusive.

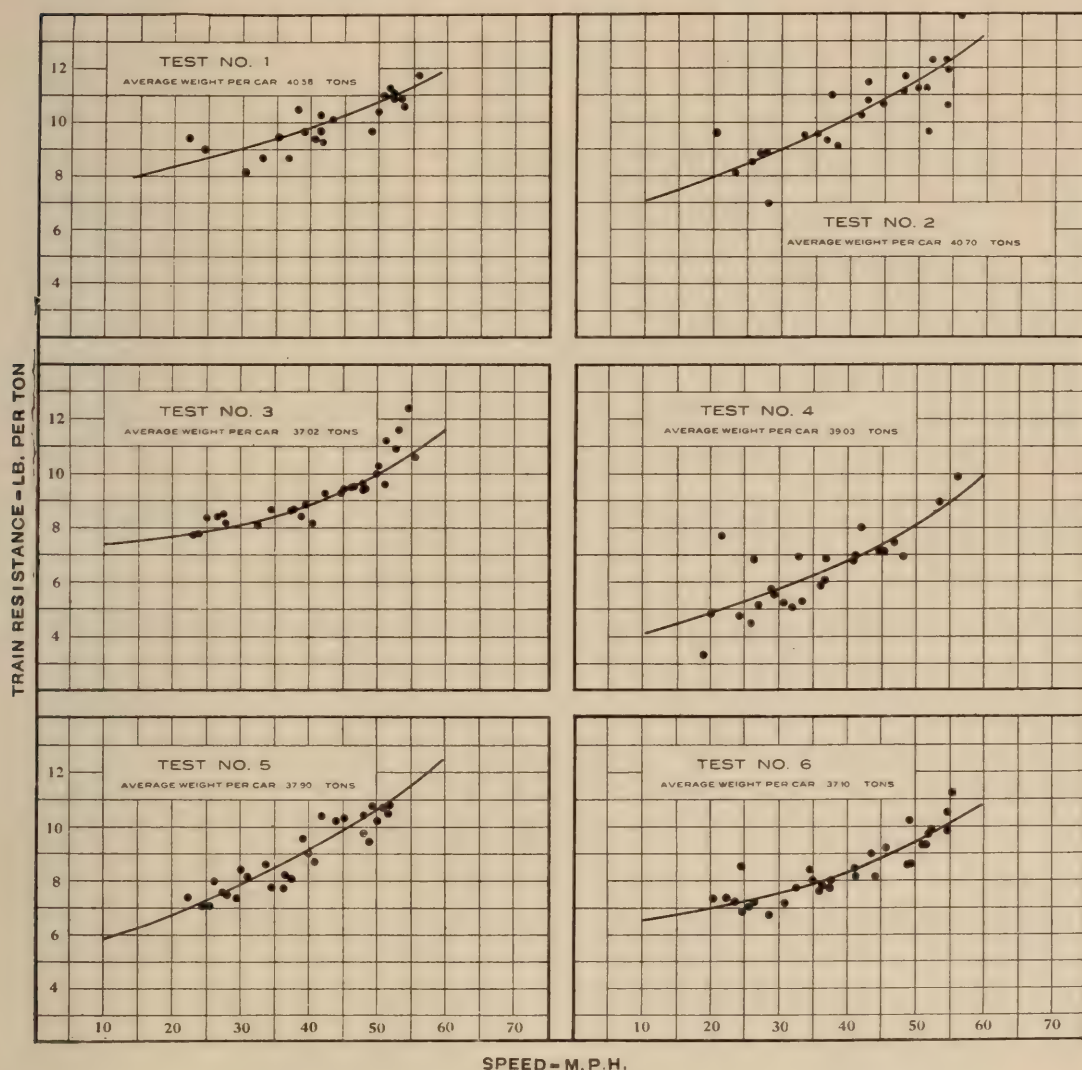


FIG. 1. DIAGRAMS SHOWING THE RELATION BETWEEN TRAIN RESISTANCE AND SPEED FOR SIX TRAINS

There is considerable variation among the points on the individual plots of Figs. 1 to 5, as well as considerable variation of the points from the mean defined by the curves. It is possible that part of this variation may be due to accumulated errors in instruments or in the

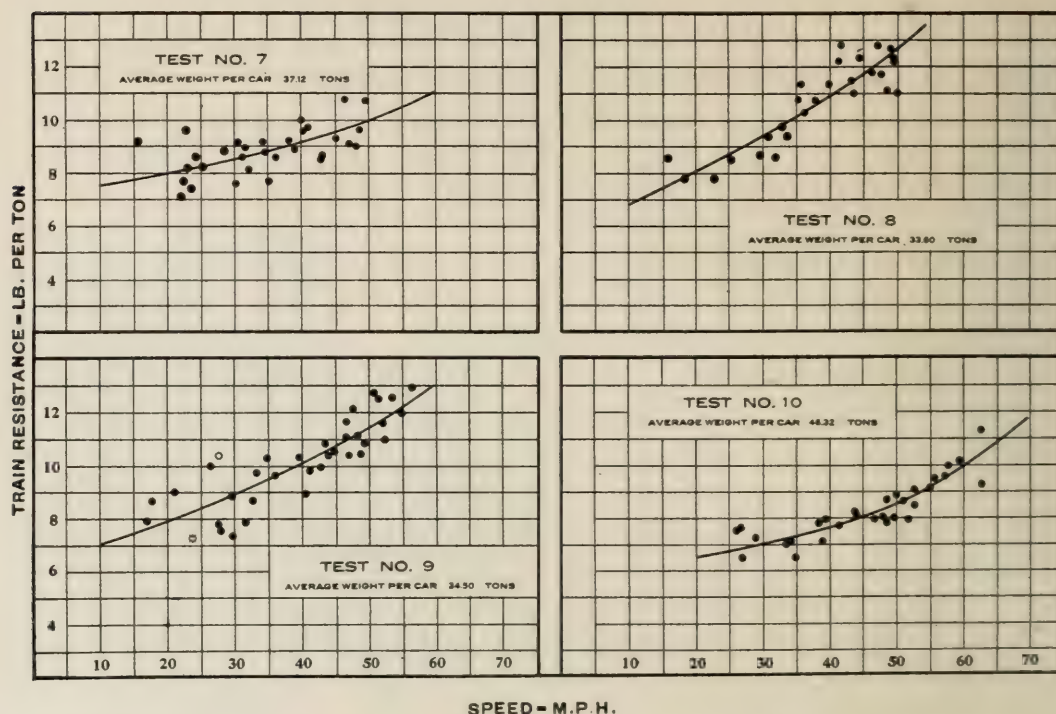


FIG. 2. DIAGRAMS SHOWING THE RELATION BETWEEN TRAIN RESISTANCE AND SPEED FOR FOUR TRAINS

calculations, but since every precaution was taken to avoid such errors, they are undoubtedly of little consequence. The data, particularly for certain tests during which wind conditions changed considerably, indicate that the usual variations in the direction and velocity of the wind during any test are sufficient to account for the differences in train resistance shown in these figures. Variations in such other components of train resistance as journal friction and oscillatory resistances are also undoubtedly accountable in a large degree for the differences discussed. The data do not afford a means of evaluating the influence of such components of resistance.

14. *Results of All the Tests.*—The twenty-eight curves from Figs. 1 to 5 have been brought together in Fig. 6 which embodies, therefore, the immediate results of all the tests. These curves make

it clear that there was a maximum variation of about 75 per cent in the resistance of different trains. Difference in wind velocity fails to account for this variation, except in a few selected cases, but there

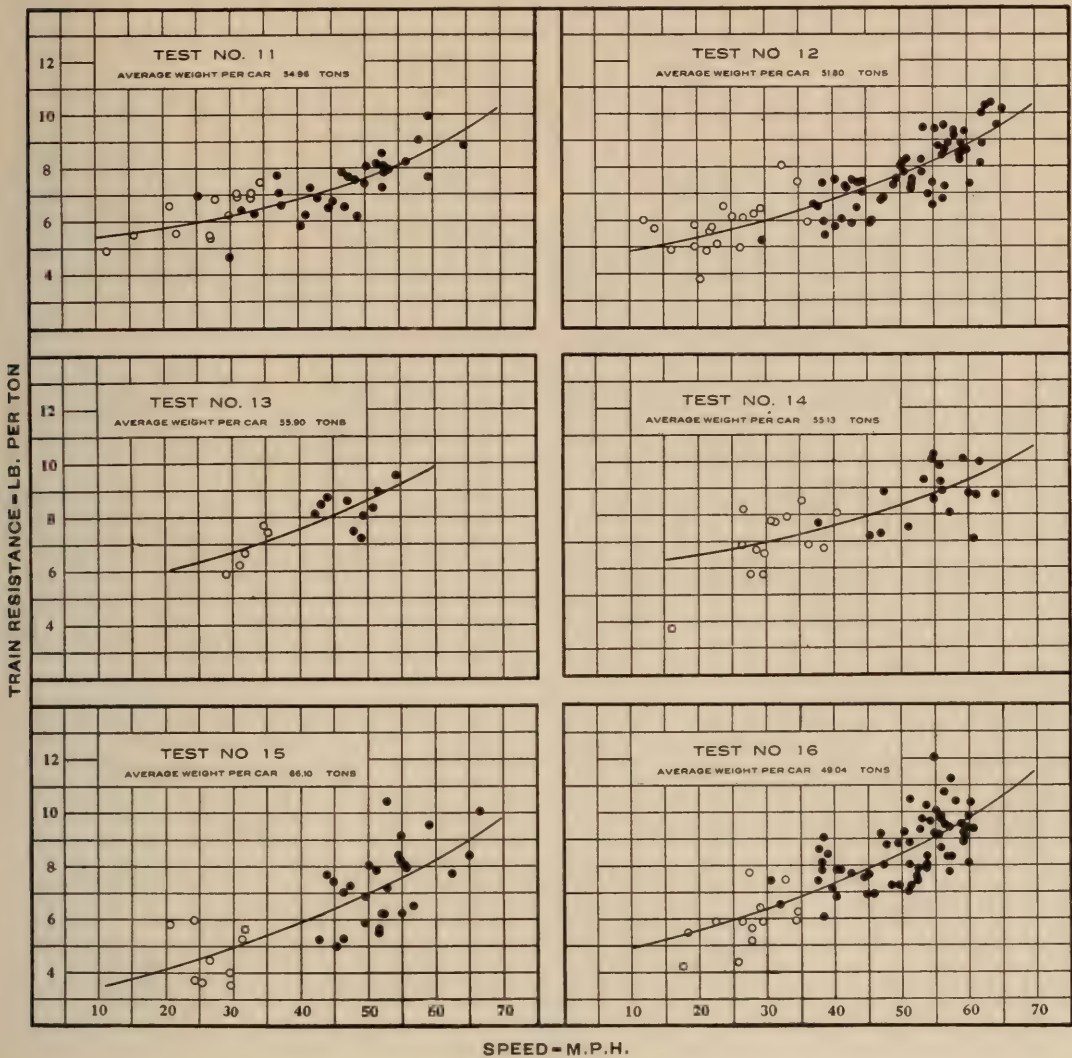


FIG. 3. DIAGRAMS SHOWING THE RELATION BETWEEN TRAIN RESISTANCE AND SPEED FOR SIX TRAINS

was every reason to believe that as in the freight train resistance tests reported in Bulletin 43 of the Engineering Experiment Station the divergence of these curves might be explained by the variation in the average weight of the cars going to make up the different trains. Comparison with the tabular data shows that the four upper curves are derived from tests of trains in which the average car weight was 36.5 tons while the four lower curves are from tests of trains in which the

average car weight was 69.8 tons. These facts serve as a rough indication of the part played by car weight in effecting changes in train resistance. As has been previously stated, this conclusion was anticipated when the work was begun and tests were made therefore with trains which cover the ordinary range of passenger car weight.

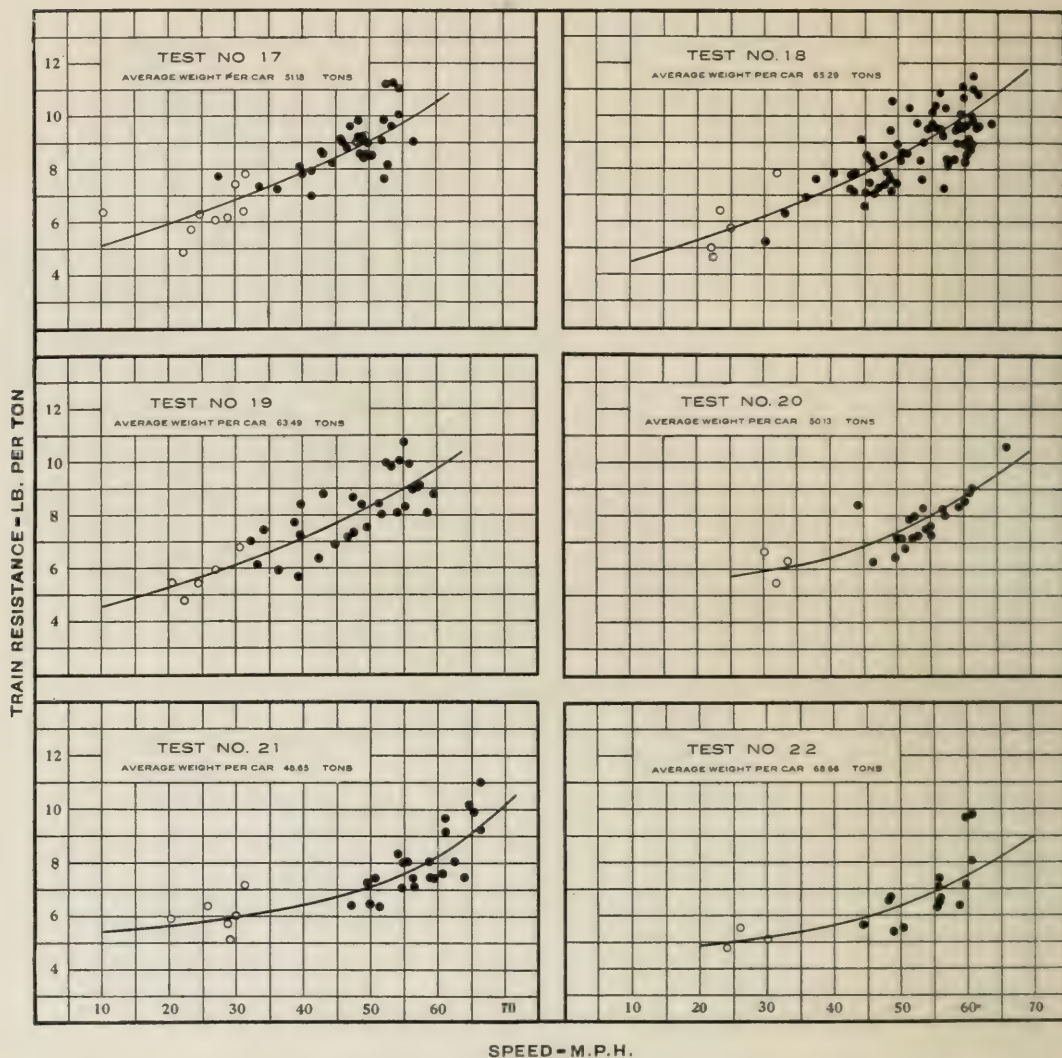


FIG. 4. DIAGRAMS SHOWING THE RELATION BETWEEN TRAIN RESISTANCE AND SPEED FOR SIX TRAINS

If in Fig. 6 at the point corresponding to 20 miles per hour a perpendicular is erected, it will cut the curves in twenty-eight points, each of which pertains to a particular train and defines for that train the average value of resistance at a speed of 20 miles per hour. If each of these resistance values is plotted with respect to the average

car weight of the train to which it pertains, the diagram for 20 miles per hour shown in Fig. 7 is obtained. Since in this diagram the values of resistance all relate to a common speed, the influence of speed on resistance is eliminated, and the figure shows the relation which at 20 miles per hour exists between resistance and average car weight. Fig.

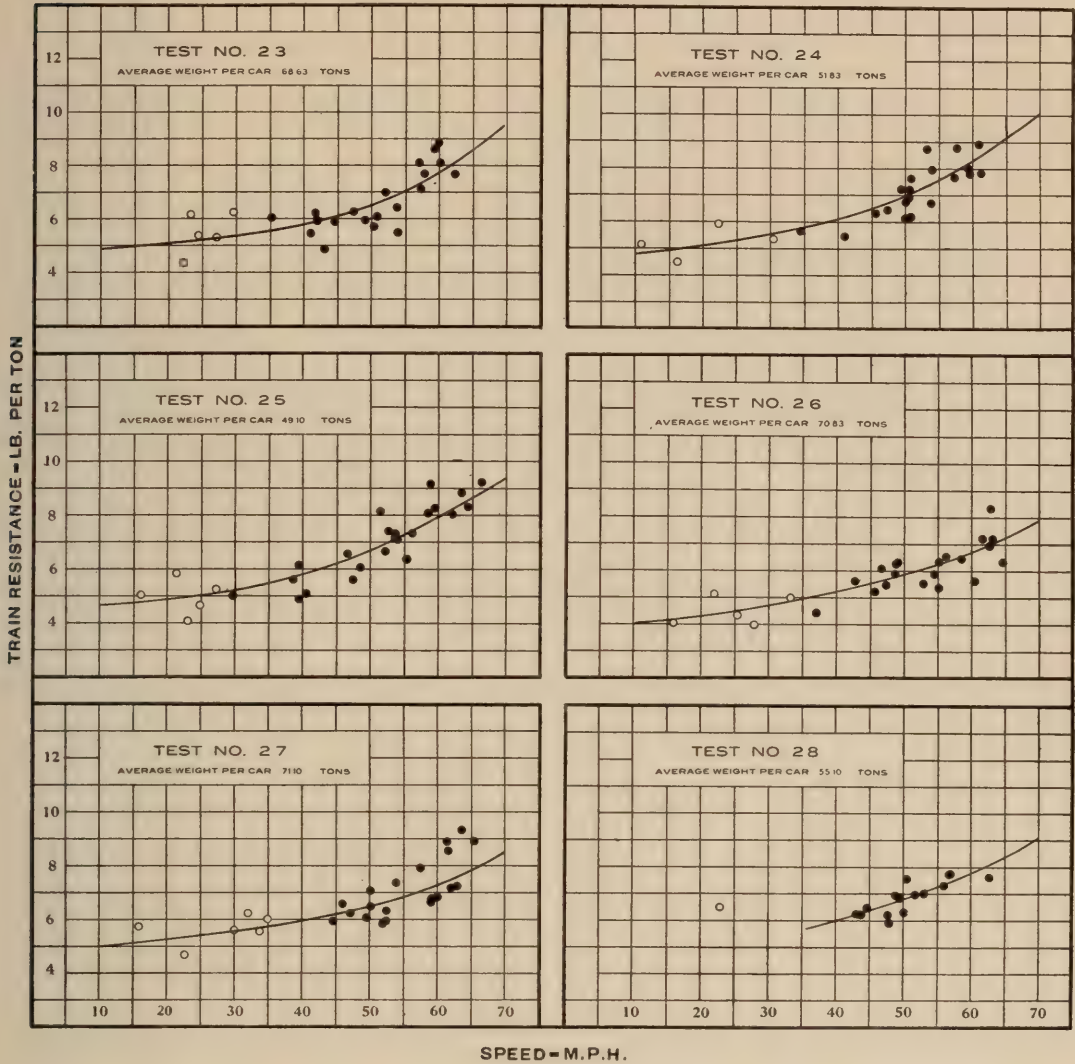


FIG. 5. DIAGRAMS SHOWING THE RELATION BETWEEN TRAIN RESISTANCE AND SPEED FOR SIX TRAINS

7 includes seven diagrams obtained by this process for speeds of 10, 20, 30, 40, 50, 60 and 70 miles per hour. The coördinates of the points plotted in Fig. 7 are given in Table 2. In it the tests are arranged in the order of the average car weights.

Both Fig. 7 and Table 2 show that the points on the individual plots fall into three groups. The group having the lowest average car weight was obtained from tests made on local train number 24 which has been described on page 12 and in Table 1. It has been noted that the number of cars in these trains having four-wheel trucks varied from 50 per cent to 80 per cent. The intermediate group of points was derived from tests with train number 5 in which the num-

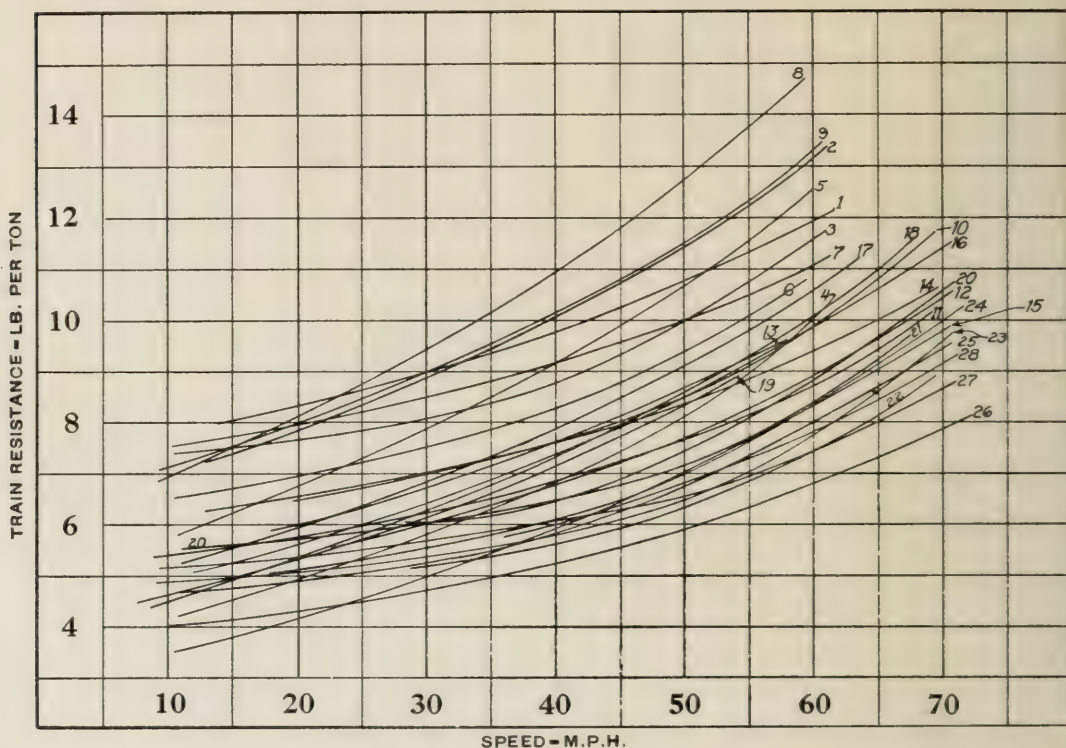


FIG. 6. CURVES SHOWING THE RELATION BETWEEN TRAIN RESISTANCE AND SPEED FOR THE TWENTY-EGT TRAINS TESTED

ber of cars having four-wheel trucks varied from 18 per cent to 27 per cent. The group of points pertaining to trains having a high average car weight applies to tests made on train number 2 in which the number of cars having four-wheel trucks varied from 0 per cent to 20 per cent.

In considering the variation among the points on the individual plots of Fig. 7 it should be borne in mind that each point represents the average resistance of a particular train at a given speed. With the exception of test number 4 which results in abnormally low resistance values the average variation of all the points from the mean

curves is 8 per cent. There are three trains which at some speed gave resistances greater than 20 per cent above or below the mean curve. The majority, however, vary from the curve by 10 per cent or less.

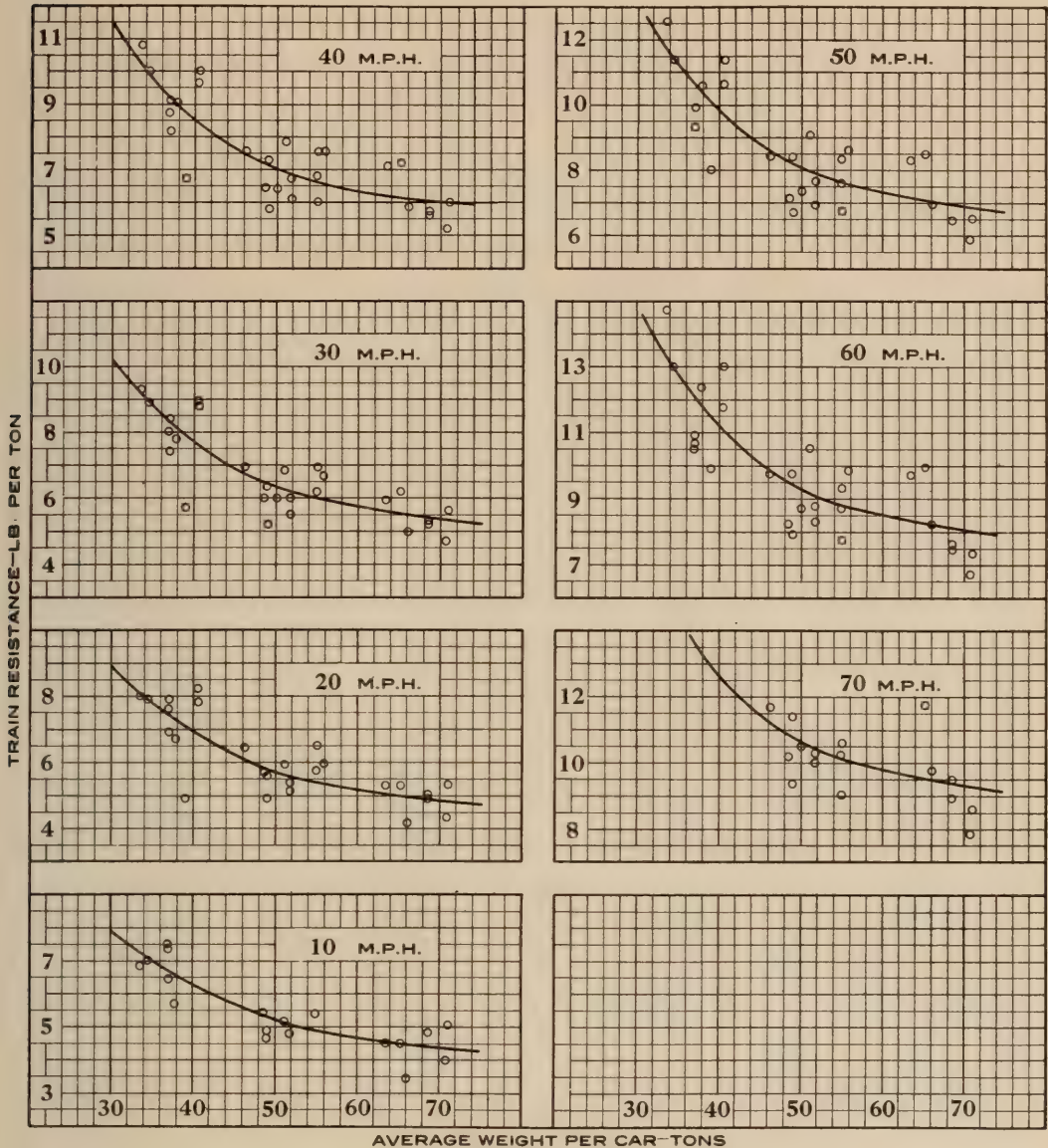


FIG. 7. DIAGRAMS SHOWING THE RELATION BETWEEN TRAIN RESISTANCE AND AVERAGE CAR WEIGHT FOR SEVEN DIFFERENT SPEEDS

In the following table are given the average deviations above and below the mean for all the points in Fig. 7.

No satisfactory explanation for these differences is obtainable from the data. They are probably due to varying external conditions

such as wind and temperature as well as to variations in train condition and make up. Variations similar to those recorded in the foregoing table may be expected with any train.

TABLE 2

VALUES OF RESISTANCE AT VARIOUS SPEEDS DERIVED FROM THE CURVES FOR THE INDIVIDUAL TESTS

This table provides the coördinates of the points plotted in Fig. 7

Test No.	Average Weight per Car Tons	Train Resistance—Pounds per Ton						
		10 M. P. H.	20 M. P. H.	30 M. P. H.	40 M. P. H.	50 M. P. H.	60 M. P. H.	70 M. P. H.
8	33.60	6.83	8.00	9.30	10.80	12.56	14.72
9	34.50	7.01	7.90	8.90	10.00	11.39	13.00
3	37.02	7.35	7.61	8.03	8.73	9.91	10.50
6	37.10	6.45	6.90	7.43	8.18	9.30	10.67
7	37.12	7.47	7.90	8.42	9.10	9.91	10.92
5	37.90	5.70	6.70	7.80	9.05	10.58	12.38
4	39.03	4.90	5.72	6.73	8.00	9.90
1	40.58	8.23	8.89	9.65	10.60	11.78
2	40.70	7.81	8.80	10.00	11.35	13.00
10	46.32	6.42	6.93	7.57	8.42	9.76	11.68
21	48.65	5.44	5.70	6.00	6.45	7.14	8.23	10.20
16	49.04	4.90	5.60	6.35	7.30	8.40	9.73	11.40
25	49.10	4.67	4.89	5.21	5.80	6.70	7.91	9.38
20	50.13	6.00	6.40	7.35	8.70	10.50
17	51.18	5.18	5.92	6.82	7.85	9.08	10.52
12	51.80	4.85	5.38	6.00	6.72	7.65	8.78	10.30
24	51.83	4.80	5.12	5.51	6.10	6.93	8.30	10.00
11	54.96	5.40	5.75	6.20	6.81	7.60	8.70	10.25
28	55.10	6.00	6.76	7.76	9.05
14	55.13	6.50	6.95	7.55	8.33	9.31	10.60
13	55.90	5.96	6.68	7.56	8.60	9.85
19	63.49	4.52	5.30	5.94	7.10	8.30	9.70
15	65.29	4.51	5.30	6.20	7.22	8.48	9.94	11.75
15	66.10	3.46	4.17	4.98	5.87	6.94	8.22	9.77
23	68.63	4.84	5.02	5.30	5.74	6.45	7.62	9.50
22	68.66	4.90	5.20	5.64	6.38	7.45	8.94
26	70.83	4.00	4.32	4.70	5.20	5.88	6.71	7.87
27	71.10	5.08	5.32	5.62	6.00	6.50	7.32	8.60

Although there is considerable variation among the points, they indicate clearly a decrease in the resistance as the car weight increases. The rate of this decrease is shown by the curves drawn to represent the points on the individual plots of Fig. 7. These curves have been drawn by the same method as the curves of Figs. 1 to 5 inclusive.

The seven curves from the individual plots of Fig. 7 have been brought together in Fig. 8, which shows, therefore, the average rela-

tion between resistance and average car weight for each of seven different speeds. Fig. 8 shows in graphical form the results of the whole research.

AVERAGE DEVIATION OF ALL POINTS IN FIG. 7 FROM THE MEAN AS SHOWN BY THE CURVES THERE DRAWN EXPRESSED AS PERCENTAGES OF THE CURVE ORDINATES

Speed.....	Miles per Hour						
	10	20	30	40	50	60	70
Points above the Curve.....	8.7	6.5	7.1	9.0	9.0	10.2	6.7
Points below the Curve.....	6.6	8.3	7.3	8.5	8.6	7.1	6.6

15. *The Results Expressed as Resistance-Speed Curves.*—Fig. 8, however, presents the relations in unusual form. Ordinarily train resistance is expressed as a curve or equation which defines the relation between resistance and speed instead of the relation between resistance and car weight as in this figure. Obviously a single curve will not suffice to express the results of these experiments in the usual form, since the influence of car weight cannot thereby be made evident. A number of curves will be required for this purpose, each of which will apply only to a particular average car weight. Fig. 9 presents such a group of resistance speed curves which have been derived directly from the lines of Fig. 8, and Fig. 9 shows, therefore, in different form, only such information as is obtainable from Fig. 8.

The relation between the two figures will be made clear by explaining the derivation of the curve in Fig. 9 applying to an average car weight of 40 tons. In Fig. 8 the ordinate corresponding to an average car weight of 40 tons cuts the seven lines there drawn at seven points, at which the mean resistance values are 6.3, 7.0, 7.7, 8.6, 9.8, 11.2, and 12.7 pounds per ton, corresponding to speeds of 10, 20, 30, 40, 50, 60 and 70 miles per hour respectively. These values are the coördinates of seven points on a resistance-speed curve applying to a car weight of 40 tons. These seven points have been plotted in Fig. 9 and define there the curve for 40 tons. The curves for 30, 35, 45, 50, 60, and 75 tons average weight per car have been derived in like manner. The curves of Fig. 9 reproduce quite exactly the facts presented in Fig. 8 and present the final results of the experiments. Three additional curves corresponding to 55, 65, and 70 tons per car which were included in the original diagram have been omitted from Fig. 9 to avoid confusion.

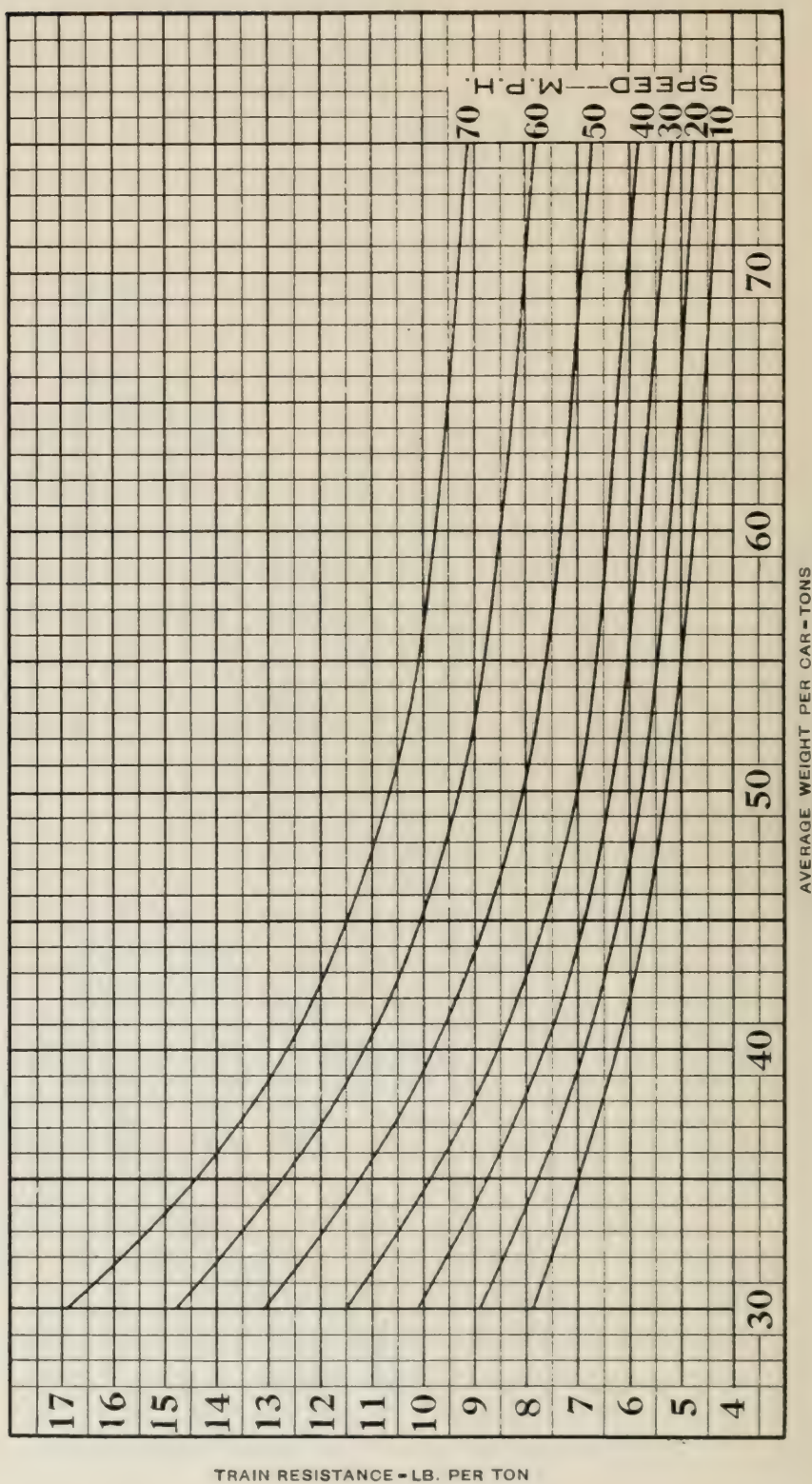


FIG. 8. CURVES SHOWING THE AVERAGE RELATION BETWEEN RESISTANCE AND AVERAGE CAR WEIGHT FOR SEVEN DIFFERENT SPEEDS

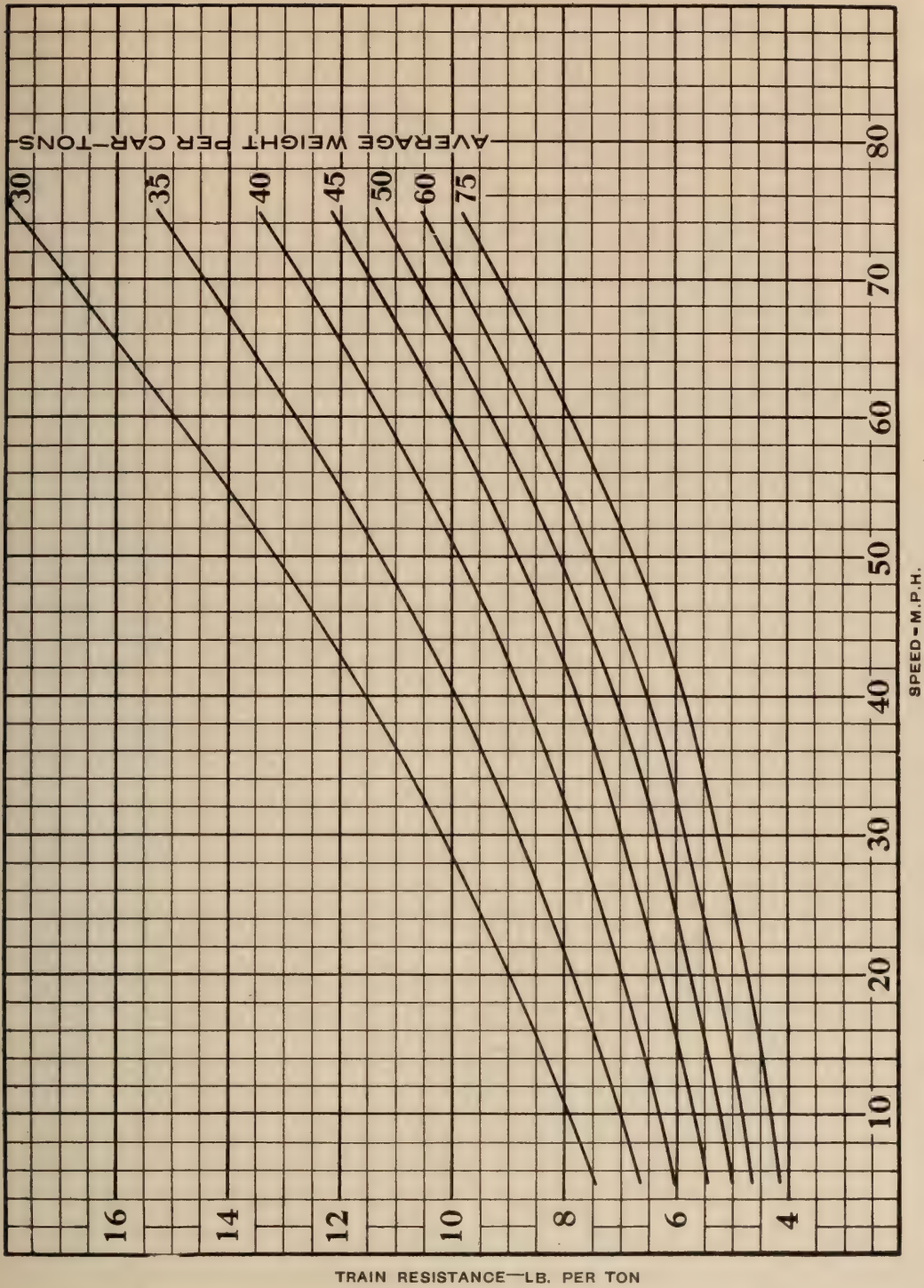


FIG. 9. CURVES SHOWING THE RELATION BETWEEN TRAIN RESISTANCE AND SPEED FOR AVERAGE CAR WEIGHT BETWEEN THIRTY AND SEVENTY-FIVE TONS

16. *The Results Expressed in Tabular Form.*—For convenience the values of resistance defined by the curves of Figs. 8 and 9 have been tabulated in Table 3 which gives the resistance values at speeds

TABLE 3
VALUES OF RESISTANCE AT VARIOUS SPEEDS AND FOR VARIOUS AVERAGE
CAR WEIGHTS

The values are derived directly from the curves of Fig. 9 and present the final results of the tests

Speed Miles per Hour	Train Resistance—Pounds per Ton										Speed Miles per Hour
	Column Headings Indicate the Average Weights per Car—Tons										
	30	35	40	45	50	55	60	65	70	75	
5	7.4	6.6	6.0	5.4	5.0	4.8	4.6	4.4	4.3	4.1	5
6	7.5	6.7	6.0	5.5	5.0	4.8	4.6	4.4	4.3	4.2	6
7	7.6	6.8	6.1	5.5	5.1	4.8	4.7	4.5	4.3	4.2	7
8	7.7	6.8	6.2	5.6	5.1	4.9	4.7	4.5	4.4	4.2	8
9	7.8	6.9	6.2	5.6	5.2	4.9	4.8	4.6	4.4	4.3	9
10	7.9	7.0	6.3	5.7	5.2	5.0	4.8	4.6	4.4	4.3	10
11	8.0	7.1	6.4	5.8	5.2	5.0	4.8	4.7	4.5	4.3	11
12	8.1	7.1	6.4	5.8	5.3	5.0	4.9	4.7	4.5	4.4	12
13	8.2	7.2	6.5	5.9	5.3	5.1	4.9	4.7	4.5	4.4	13
14	8.3	7.3	6.5	5.9	5.4	5.1	5.0	4.8	4.6	4.4	14
15	8.4	7.4	6.6	6.0	5.4	5.2	5.0	4.8	4.6	4.5	15
16	8.5	7.5	6.7	6.0	5.5	5.2	5.0	4.9	4.7	4.5	16
17	8.6	7.6	6.7	6.1	5.5	5.3	5.1	4.9	4.7	4.5	17
18	8.7	7.7	6.8	6.1	5.6	5.3	5.1	5.0	4.8	4.6	18
19	8.8	7.7	6.9	6.2	5.7	5.4	5.2	5.0	4.8	4.6	19
20	9.0	7.8	7.0	6.3	5.7	5.4	5.2	5.0	4.9	4.7	20
21	9.1	7.9	7.0	6.3	5.8	5.5	5.3	5.1	4.9	4.7	21
22	9.2	8.0	7.1	6.4	5.8	5.5	5.3	5.1	5.0	4.8	22
23	9.3	8.1	7.2	6.4	5.9	5.6	5.4	5.2	5.0	4.8	23
24	9.4	8.2	7.2	6.5	5.9	5.6	5.4	5.2	5.0	4.9	24
25	9.5	8.3	7.3	6.6	6.0	5.7	5.5	5.3	5.1	4.9	25
26	9.6	8.4	7.4	6.6	6.1	5.7	5.6	5.4	5.1	5.0	26
27	9.8	8.5	7.5	6.7	6.1	5.8	5.6	5.4	5.2	5.0	27
28	9.9	8.6	7.5	6.8	6.2	5.9	5.7	5.5	5.2	5.1	28
29	10.0	8.7	7.6	6.8	6.2	5.9	5.7	5.5	5.3	5.1	29
30	10.1	8.8	7.7	6.9	6.3	6.0	5.8	5.6	5.4	5.2	30
31	10.3	8.9	7.8	7.0	6.4	6.0	5.8	5.6	5.4	5.2	31
32	10.4	9.0	7.9	7.1	6.4	6.1	5.9	5.7	5.5	5.3	32
33	10.5	9.1	8.0	7.1	6.5	6.2	6.0	5.8	5.5	5.4	33
34	10.7	9.2	8.0	7.2	6.6	6.2	6.0	5.8	5.6	5.4	34
35	10.8	9.3	8.1	7.3	6.7	6.3	6.1	5.9	5.7	5.5	35
36	10.9	9.4	8.2	7.4	6.7	6.4	6.2	6.0	5.7	5.5	36
37	11.1	9.5	8.3	7.4	6.8	6.5	6.2	6.0	5.8	5.6	37
38	11.2	9.6	8.4	7.5	6.9	6.5	6.3	6.1	5.9	5.7	38
39	11.4	9.8	8.5	7.6	7.0	6.6	6.4	6.2	5.9	5.7	39
40	11.5	9.9	8.6	7.7	7.0	6.7	6.4	6.2	6.0	5.8	40
41	11.7	10.0	8.7	7.8	7.1	6.8	6.5	6.3	6.1	5.9	41
42	11.8	10.1	8.8	7.9	7.2	6.9	6.6	6.4	6.2	6.0	42
43	12.0	10.3	9.0	8.0	7.3	6.9	6.7	6.5	6.3	6.0	43
44	12.2	10.4	9.1	8.1	7.4	7.0	6.8	6.6	6.4	6.1	44
45	12.3	10.5	9.2	8.2	7.5	7.1	6.9	6.7	6.4	6.2	45
46	12.5	10.7	9.3	8.3	7.6	7.2	7.0	6.8	6.5	6.3	46
47	12.6	10.8	9.4	8.4	7.7	7.3	7.1	6.9	6.6	6.4	47
48	12.8	11.0	9.6	8.5	7.8	7.4	7.2	7.0	6.7	6.5	48
49	13.0	11.1	9.7	8.6	7.9	7.5	7.3	7.1	6.8	6.6	49
50	13.1	11.2	9.8	8.8	8.0	7.6	7.4	7.2	7.0	6.7	50
51	13.3	11.4	9.9	8.9	8.1	7.7	7.5	7.3	7.1	6.8	51
52	13.5	11.5	10.1	9.0	8.2	7.8	7.6	7.4	7.2	6.9	52
53	13.7	11.7	10.2	9.1	8.4	7.9	7.7	7.5	7.3	7.0	53
54	13.8	11.8	10.3	9.2	8.5	8.1	7.8	7.6	7.4	7.1	54
55	14.0	12.0	10.5	9.4	8.6	8.2	8.0	7.7	7.5	7.2	55

TABLE 3—(CONTINUED)

Speed Miles per Hour	Train Resistance—Pounds per Ton										Speed Miles per Hour
	Column Headings Indicate the Average Weights per Car—Tons										
	30	35	40	45	50	55	60	65	70	75	
56	14.2	12.1	10.6	9.5	8.7	8.3	8.1	7.8	7.6	7.3	56
57	14.4	12.3	10.8	9.6	8.9	8.4	8.2	8.0	7.7	7.5	57
58	14.6	12.5	10.9	9.8	9.0	8.6	8.3	8.1	7.8	7.6	58
59	14.8	12.6	11.1	9.9	9.1	8.7	8.4	8.2	8.0	7.7	59
60	15.0	12.8	11.2	10.0	9.2	8.8	8.6	8.3	8.1	7.8	60
61	15.1	12.9	11.3	10.2	9.4	8.9	8.7	8.4	8.2	7.9	61
62	15.3	13.1	11.5	10.3	9.5	9.1	8.8	8.6	8.3	8.1	62
63	15.5	13.2	11.7	10.5	9.7	9.2	9.0	8.7	8.5	8.2	63
64	15.7	13.4	11.8	10.6	9.8	9.3	9.1	8.8	8.6	8.3	64
65	15.9	13.6	11.9	10.7	9.9	9.5	9.2	8.9	8.7	8.4	65
66	16.1	13.8	12.1	10.9	10.0	9.6	9.3	9.1	8.8	8.6	66
67	16.3	13.9	12.2	11.0	10.2	9.7	9.4	9.2	9.0	8.7	67
68	16.5	14.1	12.4	11.1	10.3	9.9	9.6	9.3	9.1	8.8	68
69	16.7	14.3	12.5	11.3	10.5	10.0	9.7	9.5	9.2	9.0	69
70	16.9	14.4	12.7	11.4	10.6	10.1	9.9	9.6	9.4	9.1	70
71	17.1	14.6	12.8	11.6	10.7	10.3	10.0	9.7	9.5	9.2	71
72	17.3	14.8	13.0	11.7	10.9	10.4	10.1	9.9	9.6	9.4	72
73	17.5	15.0	13.1	11.9	11.0	10.6	10.3	10.0	9.8	9.5	73
74	17.7	15.1	13.3	12.0	11.2	10.7	10.4	10.1	9.9	9.7	74
75	17.9	15.3	13.5	12.1	11.3	10.8	10.5	10.3	10.0	9.8	75

between 5 and 75 miles per hour and for car weights ranging from 30 to 75 tons. Table 3 also includes the coördinates of the resistance curves corresponding to 55, 65 and 70 tons per car and omitted from Fig. 10.

17. *Final Results.*—The final results of the research are presented in the two forms just stated, namely, Fig. 9 and Table 3, from which the resistance of ordinary passenger trains may be predicted with reasonable accuracy. It should be borne in mind, however, that these results are applicable to trains running at uniform speed, on level tangent track of good construction, during weather when the temperature is not lower than 40 degrees F. and when the wind velocity does not exceed 25 m. p. h.*

It is also significant that a considerable number of the tests developed resistances averaging about 8 per cent in excess of the mean resistance which would be predicted by the use of Figs. 7, 8 or 9. It should be understood that this allowance is intended to cover probable variations in the resistance of different trains under normal op-

*Twenty-five of the tests here reported were made when the wind velocity did not exceed 20 m. p. h. During two tests it did not exceed 25 m. p. h. and during only one test did it exceed 30 m. p. h.

erating conditions. This allowance in no way takes the place of that additional reserve which must be allowed to cover unusual variations in resistance due to low temperatures, or high winds or of that reserve in tractive effort of the locomotive necessitated by operating conditions which reduce the efficiency of the locomotive itself.

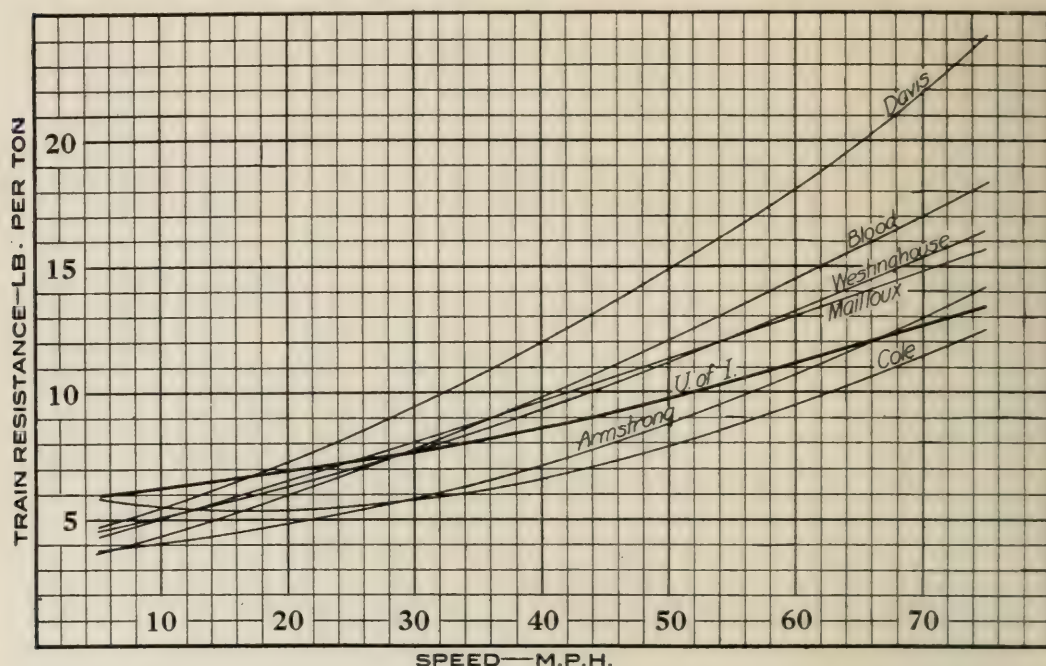


FIG. 10. COMPARATIVE CURVES SHOWING THE RELATION BETWEEN TRAIN RESISTANCE AND SPEED FOR TRAIN COMPOSED OF EIGHT 40-TON CARS

18. *Comparison with Other Experiments.*—For purposes of comparison with the results of other investigations the following formulas are given, together with Figs. 10 and 11. The curves in Fig. 10 have been calculated for a train composed of eight 40-ton cars while those of Fig. 11 have been calculated for a train of ten 60-ton cars.

$$\text{Armstrong*} \quad R = \frac{50}{\sqrt{W}} + 0.035S + \frac{0.002 a S^2}{W} \left[1 + \frac{n-1}{10} \right]$$

$$\text{Blood†} \quad R = 3 + 0.12S + \left[0.0014 + \frac{0.40}{W} \right] S^{1.8}$$

*"Standard Handbook for Electrical Engineers," Section 13, p. 947, 1910.

†Proc. Amer. Soc. Mech. Eng., Vol. 24, p. 945, 1903.

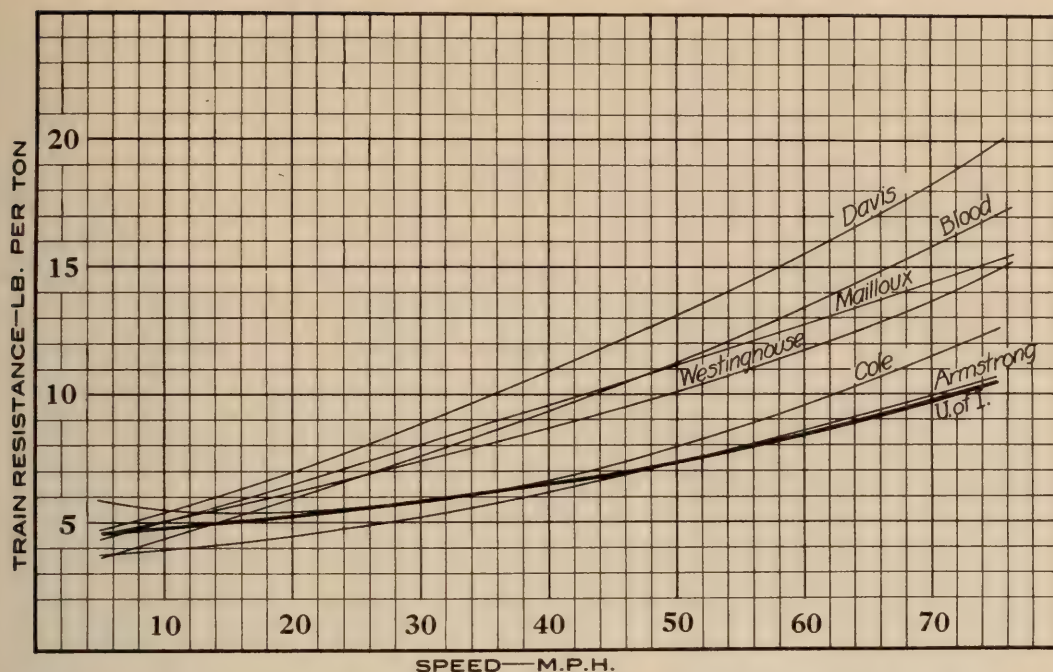


FIG. 11. COMPARATIVE CURVES SHOWING THE RELATION BETWEEN TRAIN RESISTANCE AND SPEED FOR TRAIN COMPOSED OF TEN 60-TON CARS

$$\text{Cole}^* \quad R = 5.4 + 0.002 [S - 15]^2 + \frac{100}{[S + 2]^3}$$

$$\text{Davis}^\dagger \quad R = 4 + 0.13 S + \frac{0.33 S^2}{W} \left[1 + \frac{n-1}{10} \right]$$

$$\text{Mailloux}^\ddagger \quad R = 3.5 + 0.15 S + \left[\frac{(0.02 N + 0.25)}{N W} \right] S^2$$

$$\text{Westinghouse}^\S \quad R = 4 + \frac{S}{10} + \frac{10 S^2}{36 W}$$

Notation: R = train resistance, pounds per ton.

S = speed, miles per hour.

W = weight of the train, tons.

N = number of cars in the train.

A = cross sectional area.

*Railway Age Gazette, Vol. 47 n. s., pp. 361, 411, 451, 503, 546, 583, 1909.

†Street Railway Journal, Vol. 24, p. 1003, 1904.

‡Proc. Amer. Inst. Elec. Eng., Vol. 23, p. 731, 1904.

§Westinghouse Company.

APPENDIX

TYPICAL TABLES OF RESULTS OF THE INDIVIDUAL TESTS

In this appendix three tables are given, each of which shows the principal results of the calculations for one test. The tests have been chosen so that each one is fairly representative of all the tests made with a particular class of train. Table 4, for example, is typical of the results obtained with train No. 24, Table 5 representative of the tests with train No. 5, and Table 6 representative of the tests with train No. 2. The final values of net resistance on tangent, level track, at uniform speed are given in column 12, and the corresponding values of speed in column 11. These two columns give the coördinates of the points plotted on the individual diagrams of Figs. 1 to 5, inclusive.

It has been customary in bulletins of the Engineering Experiment Station of this nature to present complete tables of data for all the tests. This practice has been maintained largely for the purpose of showing the range of conditions such as wind velocity and direction, acceleration, grade and length of sections. It has also served to show the division of the gross train resistance into such items as acceleration, grade, and net resistance. In view of the fact that these data have been given so fully in previous publications and since the relation between the various items is not materially different in this case, it is thought that the presentation of typical tables of data is sufficient.

TABLE 4
THE RESULTS OF TEST NO. 7

Method of Calculation	Item No.	Length of Section Feet	Total Drawbar Pull Pounds	Acceleration Miles per Hour per Second	Speeds		Grade + Up - Down Feet per Mile	Wind		Speed m. p. h.	Net Train Resistance Pounds per Ton
					At Entrance to Section m. p. h.	At Exit from Section m. p. h.		Approximate Direction	Approximate Velocity m. p. h.		
1	2	3	4	5	6	7	8	9	10	11	12
Section	1	1380	7060	00.00	24.05	- 1.15	+60° R	16	15.7	9.13
	2	2700	4650	24.05	35.45	- 4.30	+60° R	16	30.7	9.10
	3	3564	3510	35.45	43.90	- 9.90	+60° R	16	40.6	9.52
	4	4112	2975	43.90	48.00	- 2.80	+60° R	16	46.7	10.68
	5	4744	2675	48.00	51.55	- 3.90	+60° R	16	49.8	10.66
"	6	1008	6520	18.50	25.50	+11.00	+50° R	12	22.9	9.56
	7	2800	4925	25.50	35.90	+ 4.30	+50° R	12	31.8	8.92
	8	3532	3925	35.90	42.90	+ 0.70	+50° R	12	40.2	9.93
	9	4160	2900	42.90	48.32	- 4.70	+50° R	12	47.3	9.07
	10	4260	2275	48.32	48.00	+10.00	+50° R	12	48.4	8.97
"	11	2144	4650	17.60	29.25	- 3.40	+60° R	12	24.4	8.53
	12	3024	3580	29.25	37.70	- 7.70	+60° R	12	34.4	9.12
	13	3628	2825	37.70	43.25	- 8.30	+60° R	12	41.2	9.68
	14	2036	4790	15.75	28.05	- 2.30	+35° R	10	23.2	8.12
	15	2840	3540	28.05	34.45	+ 3.00	+35° R	10	32.3	8.07
"	16	3204	2860	34.45	37.40	+ 5.90	+35° R	10	36.4	8.53
	17	2524	4960	21.80	33.25	+ 1.30	+40° R	10	28.7	8.78
	18	3368	3850	33.25	40.92	- 0.60	+40° R	10	38.3	9.17
	19	2240	5475	17.65	30.25	+ 6.60	+25° R	9	25.5	8.15
	20	3052	4165	30.25	37.20	+ 7.60	+27° R	9	34.7	8.71
"	21	1948	4830	14.40	27.25	- 0.80	+60° R	10	22.1	7.07
	22	2760	3540	27.25	33.60	+ 1.90	+60° R	10	31.4	8.56
	23	3196	3050	33.60	37.40	+ 7.60	+60° R	10	35.3	7.63
	24	3448	2710	37.40	40.10	+ 4.00	+60° R	10	39.2	8.83
	25	3796	2325	41.95	43.25	+ 5.30	+60° R	10	43.1	8.47
"	26	1984	5020	15.85	26.55	+ 9.00	+45° R	8	22.6	7.63
	27	2676	3925	26.55	32.95	+ 9.50	+45° R	8	30.4	7.55
	28	3820	2425	40.95	44.40	- 2.50	+50° R	10	43.4	8.61
	29	3664	2250	44.40	46.25	- 0.90	+50° R	10	45.5	9.25
	30	4292	1950	46.25	49.00	- 8.90	+50° R	10	48.9	9.59
"	31	2084	4830	15.85	28.40	0.00	+25° R	7	23.7	7.37

TABLE 5
THE RESULTS OF TEST No. 24

Method of Calculation	Item No.	Length of Section Feet	Total Drawbar Pull Pounds	Acceleration Miles per Hour per Second	Speeds		Grade + Up — Down Feet per Mile	Wind		Speed m. p. h.	Net Train Resistance Pounds per Ton
					At Entrance to Section m. p. h.	At Exit from Section m. p. h.		Approximate Direction	Approximate Velocity m. p. h.		
1	2	3	4	5	6	7	8	9	10	11	12
Point	3	10630	+1.528	— 1.32	+15° L	3	16.20	4.50
"	4	18030	+2.745	+ 0.79	+40° R	6	11.00	5.15
"	5	13750	+2.185	— 7.04	+40° R	6	22.30	5.91
"	6	8600	+1.330	— 7.74	+40° R	6	30.40	5.36
Section	1	4484	5400	50.45	51.90	+ 2.51	0°	8	50.90	6.20
"	2	5200	6150	49.00	53.40	— 6.10	+10° R	18	50.60	6.96
"	3	2968	4840	57.50	58.65	— 9.18	+10° R	24	57.80	8.79
"	4	4812	4000	60.20	60.80	— 5.01	+5° R	24	59.60	7.86
"	5	1788	500	61.70	61.70	—14.60	+5° R	23	61.30	6.42
"	6	3676	5700	49.90	51.30	+ 1.48	+10° R	22	50.10	6.74
"	7	3676	5600	51.15	51.00	+10.46	+10° R	22	50.10	6.15
"	8	3964	6480	54.75	54.75	+ 7.37	+10° R	20	54.00	8.56
"	9	4016	7300	45.35	47.10	+ 9.67	+20° R	18	45.60	6.33
"	10	4120	6890	50.80	52.80	+ 2.27	+20° R	20	51.00	7.67
"	38	1560	5000	52.40	52.80	— 0.74	0°	8	53.20	9.68
"	39	2084	7150	46.40	48.85	— 4.33	+10° R	18	47.40	6.47
"	40	1976	5250	55.10	55.30	— 0.83	+15° R	22	53.90	6.73
"	41	2180	2400	60.50	60.50	—10.12	+5° R	24	59.40	8.04
"	42	1788	2100	60.80	61.40	—21.84	+5° R	23	61.00	8.94
"	43	2412	600	40.45	42.40	+ 0.57	+10° R	17	41.10	5.48
"	44	2028	8400	38.65	41.10	+ 6.04	+15° R	31	34.50	5.67
"	45	2972	6740	51.30	50.80	+15.47	+20° R	20	50.70	7.23
"	46	1816	7040	50.80	50.60	+14.85	+20° R	20	49.50	7.27
"	47	2944	4970	57.70	58.15	+ 2.74	+20° R	20	57.40	7.68

TABLE 6
THE RESULTS OF TEST NO. 19

Method of Calculation	Item No.	Length of Section Feet	Total Drawbar Pull Pounds	Acceleration Miles per Hour per Second	Speeds		Grade + Up — Down Feet per Mile	Wind		Speed m. p. h.	Net Train Resistance Pounds per Ton
					At Entrance to Section m. p. h.	At Exit from Section m. p. h.		Approximate Direction	Approximate Velocity m. p. h.		
1	2	3	4	5	6	7	8	9	10	11	12
Point	1		15800	+ .1610			+12.66	+15° R	13	22.40	4.78
"	2		15180	+ .1920			0.00			24.40	5.40
"	3		12150	+ .1626			— 7.92	+65° R	12	30.60	6.78
"	4		12850	+ .1832			— 7.92	+45° R	5	27.00	5.94
"	8		16330	+ .2258			— 2.64	+85° R	29	20.50	5.46
Section	1	820	6310		55.60	55.60	0.00	+25° R	24	55.90	9.92
"	2	1444	10310		36.20	37.85	+13.08	+25° R	19	39.40	5.68
"	3	1224	13230		29.40	32.30	+12.05	+30° R	14	33.20	6.12
"	4	3640	8500		46.90	49.00	+ 5.28	+25° R	24	49.65	7.53
"	5	1556	9850		40.00	41.95	+ 5.36	+30° R	19	42.49	6.35
"	6	3772	9900		35.40	40.00	+ 5.18	+30° R	19	39.60	7.25
"	7	1336	10380		33.00	35.40	+ 5.38	+30° R	19	36.40	5.90
"	8	3808	7700		49.60	49.80	+ 9.90	+30° R	24	51.90	8.01
"	9	3772	7380		49.00	49.60	+ 5.51	+25° R	20	51.45	8.43
"	10	2800	8180		45.60	46.60	+ 8.54	+30° R	22	47.72	7.35
"	11	5152	8380		45.60	44.40	+19.80	+30° R	21	46.85	7.18
"	12	1572	9500		40.30	42.00	0.00	+25° R	21	42.93	8.78
"	13	1256	12500		30.10	33.60	0.00	+15° R	13	34.20	7.43
"	14	5248	6250		57.70	58.40	0.00	+30° R	23	59.50	8.78
"	15	6016	6620		55.90	57.70	0.00	+30° R	23	58.60	8.07
"	16	5900	6940		55.30	55.70	+ 3.58	+40° R	20	57.30	9.06
"	17	4148	7150		53.80	55.30	0.00	+40° R	20	56.40	8.94
"	18	4296	7800		49.70	53.40	—10.00	—70° R	19	53.30	9.87
"	19	3228	8720		44.90	49.40	—10.01	—70° R	19	48.90	8.42
"	20	1316	9600		40.90	43.60	—10.02	+65° R	12	44.90	6.89
"	21	1420	10920		34.80	38.30	— 7.92	+65° R	12	38.75	7.73
"	22	2840	6300		53.00	54.10	— 3.24	+65° R	17	55.30	8.30
"	23	2400	6940		51.70	53.00	— 7.96	+65° R	17	54.50	10.02
"	24	4364	6880		53.00	51.00	+16.00	+40° R	21	54.15	8.06
"	25	2828	6800		53.20	53.20	0.00			55.10	10.73
"	26	3856	7180		50.60	50.20	+ 5.50	+60° R	21	52.40	9.98
"	27	2440	8150		45.00	46.60	0.00	+80° R	20	47.50	8.68
"	28	3256	8330		41.10	44.40	— 4.93	+70° R	15	44.40	9.02
"	29	1748	9400		36.40	39.80	—10.02	+70° R	15	39.75	8.38
"	30	2132	11950		27.10	33.80	— 3.61	+65° R	12	32.30	7.01

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